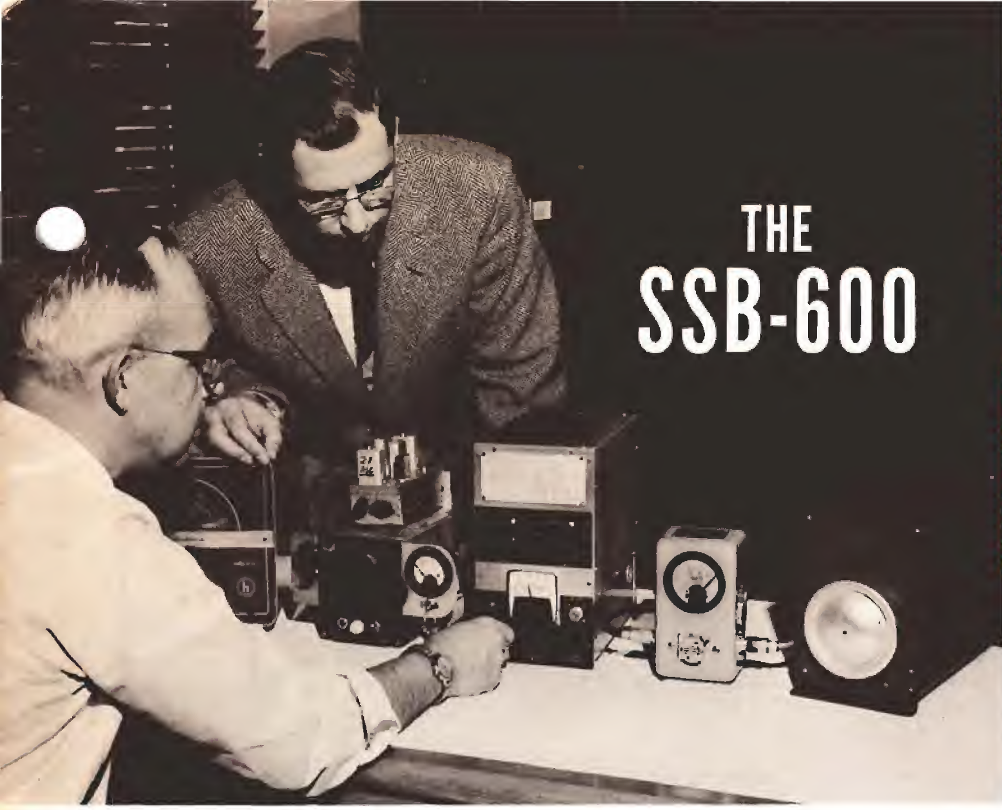
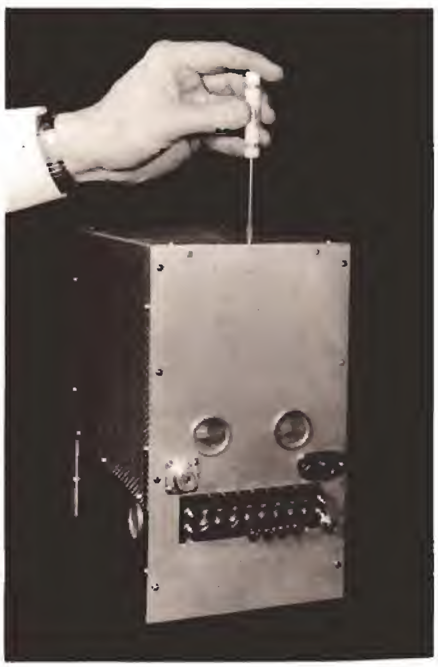
MARCH-APRIL, 1961

G-E TUBES HAM NEWS




W8DLD and W8WFH (right) run the SSB-600 linear amplifier through power-output tests. Equipment includes SSB exciter (left), modified BC-453 Command Set receiver, SSB-600 amplifier, and commercially-made r.f. wattmeter and dummy antenna load. W8DLD is supervisor of the Electronics Laboratory at General Electric's Cuyahoga Lamp Plant; and W8WFH, William C. Louden, is technical counselar in Discharge Advance Engineering at G. E.'s Large Lamp Department, both at G. E.'s Nela Park in Cleveland, Ohio. W8DLD and W8WFH recently authored the **G-E HAM NEWS** series of articles on high-power Mobile Radio Systems, including Power Supply Ideas, Crystal Controlled Converters and a BC-453 Command Set receiver conversion, and a high-power Mobile Linear Amplifier with two GL-4D21/4-125-A's in parallel.

**CLOSEUP FRONT VIEW** of the SSB-600 amplifier. Note complete operating instructions at top of panel (see copy on page 7). Markings for panel controls were engraved on black plastic name plate material.



**REAR VIEW** of the amplifier. Locations for $J_3$, $J_1$, the high voltage connector, and terminal strip $TS_1$ can be determined from this view. Note ventilating snap-in buttons on sides and back.

# GROUNDED-GRID LINEAR AMPLIFIER

## — 600 Watts DC Input in 600 Cubic Inches

By A. F. Prescott, W8DLD

**FEATURES —**

1. Efficient high frequency pi-network output circuit;
2. Complete metering of each tube;
3. Two GL-814 pentodes in zero-bias triode connection;
4. Rugged, compact construction for mobile service;
5. Covers 3.5 to 30 megacycles;
6. Only 6 x 10 x 10 inches in size.

You probably remember the old saying, "Do as I say, not as I do." W8DLD has been *saying* how to build this mobile SSB linear amplifier for years, after first constructing a model from *junk-box* parts. He recently has been *doing*, instead of saying, however, by constructing a new — and much prettier — model of his amplifier especially for this publication.

Over five years of testing in mobile and fixed service have been chalked up by the original model. It has several worthy electrical and mechanical features that make it stand out from being "just another linear amplifier."

**THE GL-814 BEAM PENTODE** was chosen for an amplifier tube because, when connected as a triode (control, screen and suppressor grids all connected together and returned to the filament) it exhibits zero bias characteristics and draws only 25 milliamperes of plate current with 2,000 plate volts applied. Since the rated plate dissipation of the GL-814 is 70 watts in ICAS[1] service, it was decided to connect two tubes in parallel to obtain about 600 watts DC input

[1]Intermittent Commercial and Amateur Service ratings.

(continued on page 2)

IN THIS ISSUE

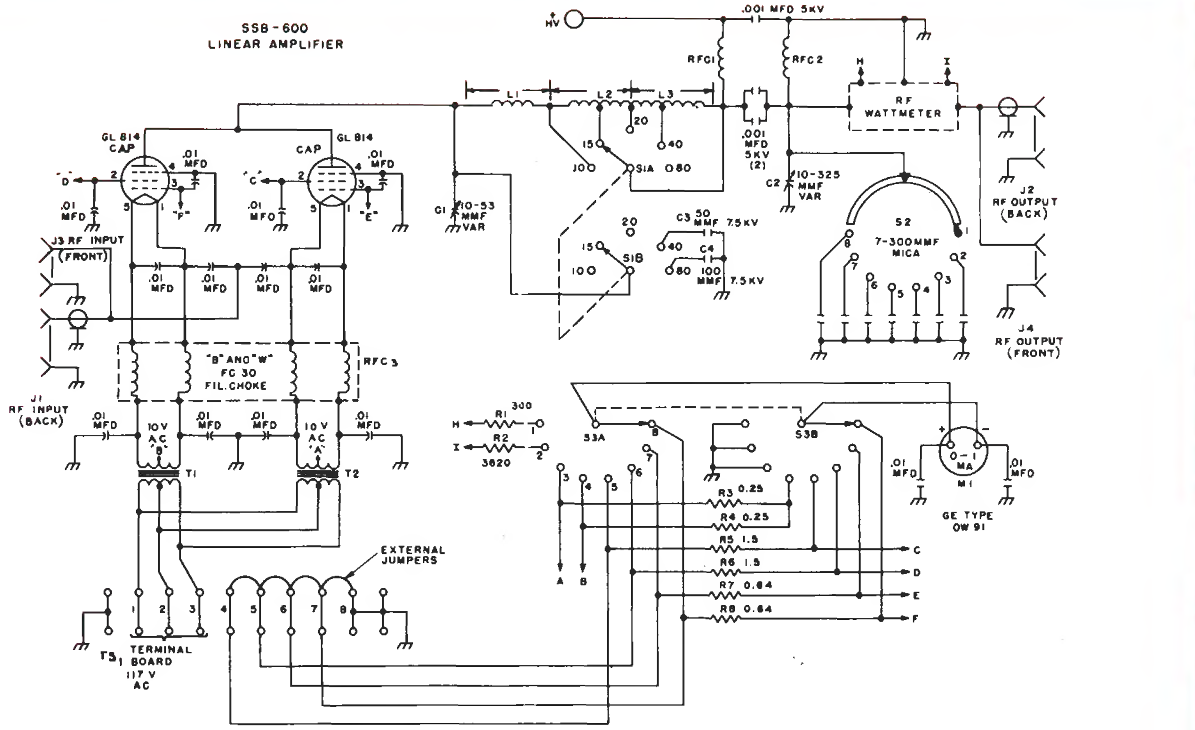



**FIG. 1. SCHEMATIC DIAGRAM** for the SSB-600 grounded-grid linear amplifier. Note the dual r.f. input ($J_1$ and $J_3$) and output ($J_2$ and $J_4$) jacks; one set of each is on the front and rear panels. The extra set is handy for picking up samples of the input and output signals for testing. The three 0.001-mfd. 5-KV capacitors in the plate circuit for DC blocking and bypassing are Centralab type 858S-1000 cylindrical ceramic capacitors. If separate metering of currents drawn by each tube is not necessary, a single 10-volt, 7-ampere filament transformer, and B & W FC-15 single filament r.f. choke can be used in place of the components shown. All bypass capacitors are 600-volt working disc ceramics, unless otherwise marked. Use terminals 1 and 2 on $TS_1$ for 105-volt AC input to the filament transformers.

**SSB-600** (continued from page 1)

capability in the low duty-cycle SSB and CW classes of service.

The grounded-grid circuit was selected because it eliminates a tuned input circuit in the linear amplifier. Also, sufficient driving power was available — about 40 to 50 watts — to drive the two GL-814 tubes in a grounded-grid, triode connected circuit, to full output. Driving power is fed directly into each side of each GL-814 filament through 0.01-mfd. disc ceramic capacitors, as shown in the schematic diagram, Fig. 1. A commercially made filament choke isolates r.f. energy from the filament transformers, $T_1$ and $T_2$. Cathode input impedance is 100 to 200 ohms, depending on frequency.

The plate circuit is a pi network, with high voltage series fed through an r.f. choke ($RFC_1$). This permits more inductance to appear in the pi network on 28 megacycles. When parallel feed is used for plate voltage application the distributed capacitance of the r.f. choke and DC blocking capacitor appear as a part of the input capacitance across the pi network, which is very undesirable.

When the output capacitance of the amplifier tubes is added to this input capacitance, it often is impossible to realize a desirable tank circuit "Q" on 28, and sometimes even on 21 megacycles. The need for parasitic chokes in the tube plate leads also is eliminated.

This circuit also has been tested with four tubes connected in parallel without encountering parasitic oscillation. The only precaution was to use four tube plate leads of equal length to the common point of parallel connection.

Bandswitching of the pi-network circuit was achieved with a tap switch ($S_{1A}$) to short out sections of the inductance ($L_1$, $L_2$ and $L_3$) as required. The input tuning capacitor of the pi network ($C_1$) has only 50-mmf maximum capacitance, and is used alone for 14, 21 and 28 megacycles. Another section of the bandswitch ($S_{1B}$) adds a 50-mmf fixed vacuum capacitor ($C_3$) for 7 megacycles, and a 100-mmf vacuum capacitor ($C_4$) for 3.5 megacycles. This system permits selecting a tuning capacitor with low minimum capacitance and good ease of tuning for the higher frequencies, and still have sufficient capacitance for good circuit "Q" at 7 and 3.5 megacycles.


TUBES

HAM NEWS

G-E HAM NEWS **presents HOW-TO-DO-IT IDEAS from the 999 radio amateurs at GENERAL ELECTRIC**

A bi-monthly publication of the RECEIVING TUBE DEPARTMENT
Owensboro, Kentucky, U. S. A. • Editor — E. A. Neal, W4ITC

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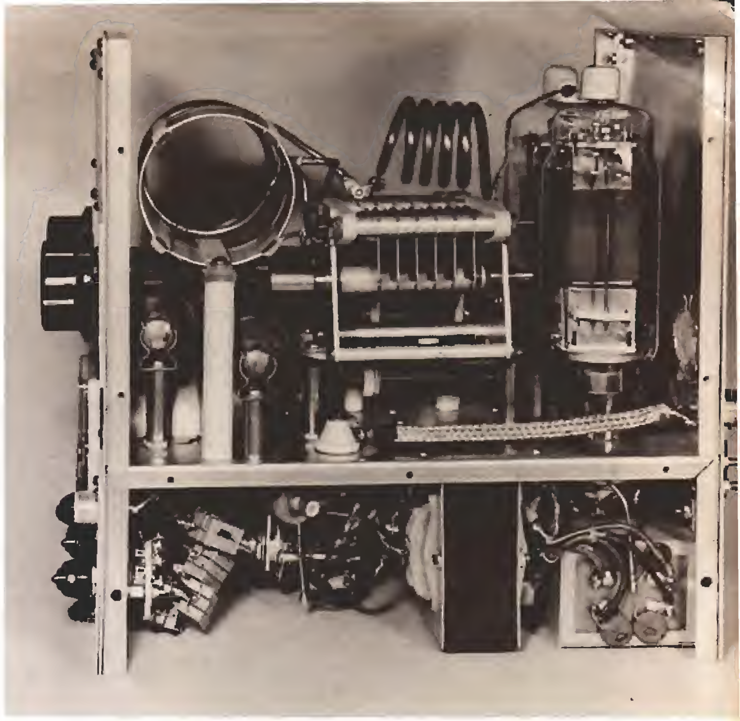
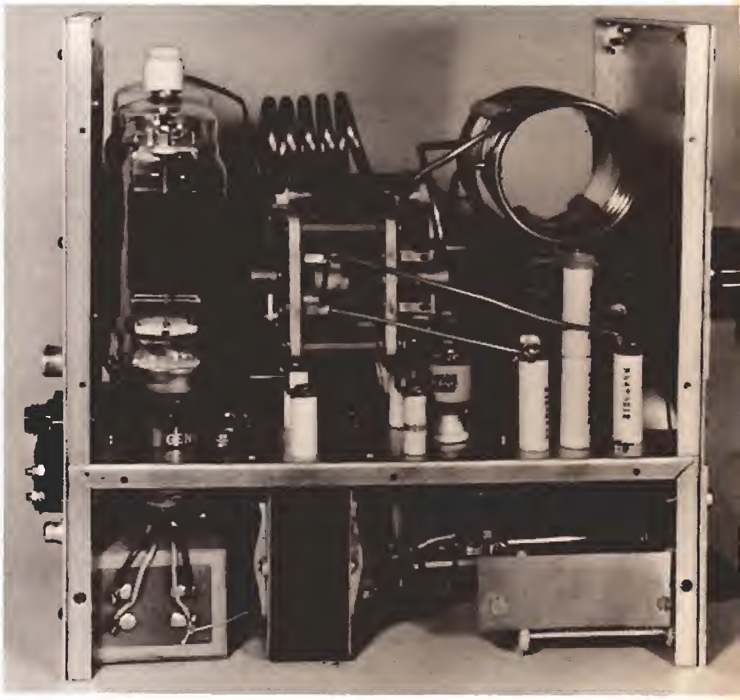
## TABLE I — PARTS LIST

$C_1$.....10-53-mmf variable, 0.125-inch air gap (Johnson 50E45, Cat. No. 154-12).
$C_2$.....10-325-mmf variable, 0.025-inch air gap (Hammarlund MC-325-M, or equivalent).
$C_3$.....50-mmf, 7,500-volt fixed vacuum capacitor (G. E. 1L38, or equivalent).
$C_4$.....100-mmf, 7,500-volt fixed vacuum capacitor (G. E. 1L33, or equivalent).
$J_1$, $J_2$......midget one-pin phono type connectors.
$J_3$, $J_4$......chassis type coaxial jack. (SO-239).
$L_1$......0.65 uh., 5 turns, 3/16-inch diameter copper tubing, 1¼ inches inside diameter, 1¾ inches long (28-Mc. coil).
$L_2$......2 uh., 5 turns, ⅛-inch diameter copper tubing or wire, 2¼ inches inside diameter, ¾ of an inch long, tapped at 2 turns from $L_1$ end (14 & 21-Mc. coil).
$L_3$......9 uh., 14 turns, No. 12 tinned copper wire, 2½ inches in diameter, 2⅜ inches long, tapped at 5 turns from $L_2$ end (7 & 3.5 megacycles) (B & W No. 3905-1 coil stock, or equivalent).
$M_1$....0—1-milliampere DC meter, 2½-inch square flange (G. E. DW-91).
$R_1$.....300 ohms, 1 watt total, precision type.
$R_2$.....3620 ohms, 1 watt, precision type.
$R_3$, $R_4$......0.25 ohms, 1 watt, precision type.
$R_5$, $R_6$......1.5 ohms, 1 watt, precision type.
$R_7$, $R_8$......0.64 ohms, 1 watt, precision type.
$RFC_1$..100-uh. solenoid type single layer r.f. choke; 140 turns of No. 26 enameled wire closewound 2½ inches long on ¾-inch diameter ceramic pillar 3 inches long.
$RFC_2$..2.5-mh, 250-milliampere pi-wound r.f. choke (National R-300, or equivalent).
$RFC_3$..Dual 15-ampere filament r.f. choke (B & W FC-30).
$S_1$..... 5-position, 2 pole, heavy-duty rotary tap switch (Shallcross type 12609[2] or Radio Switch Corp. No. 86 Standard).
$S_2$.....10-position, 1 pole, progressive shorting rotary tap switch (Centralab No. 2042).
$S_3$..... 8-position, 2 pole rotary tap switch (Centralab No. 1413, 11 positions).
$T_1$ $T_2$......10-volt, 4-ampere filament transformer, 115-volt primary (Stancor P-5016, or P-6458; Thordarson T-21F18).

[2]Shallcross Manufacturing Co., Selma, North Carolina. See manufacturers' representatives listing in Electronics Buyers Guide for nearest distributor.



**LEFT SIDE VIEW,** showing how $C_3$, $C_4$, $RFC_2$ and $S_1$ are mounted on ceramic pillars. Coils $L_2$ and $L_3$ are cemented to plastic strips supported on ceramic pillars.



**RIGHT SIDE VIEW,** showing metal pillars for grounded ends of $C_3$ and $C_4$. Insulated shafts are used for $C_1$ and $S_1$ extensions to the panel knobs. GL-814 tube sockets are sub-mounted ½ inch on pillar insulators.

The same reasoning was applied to the loading capacitance ($C_2$). A 10 to 325-mmf variable is used for the higher frequencies, and additional capacitance, up to 2,100 mmf, is cut in by $S_2$ in steps of 300 mmf. $RFC_2$ is a safety choke.

**THE METERING CIRCUIT** provides for measuring control and screen grid, and cathode currents in each GL-814 individually. This permits selecting a matched pair of GL-814's (if you happen to have spares around), and is also handy for insuring that each tube is sharing the load.

It also allows you to catch a tube starting to go bad before it has a chance to wreck its mate. Many poor signals are caused by weak tubes, causing the other tubes in parallel to be overloaded or to work under improper loading conditions.

Control grid (No. 1 grid) current is normally considered of great importance. This amplifier also has number two grids metered independently. A "look-see" in this circuit is not only interesting but educational. This eliminates guessing as to the division of the drive between the control grid and screen grid.

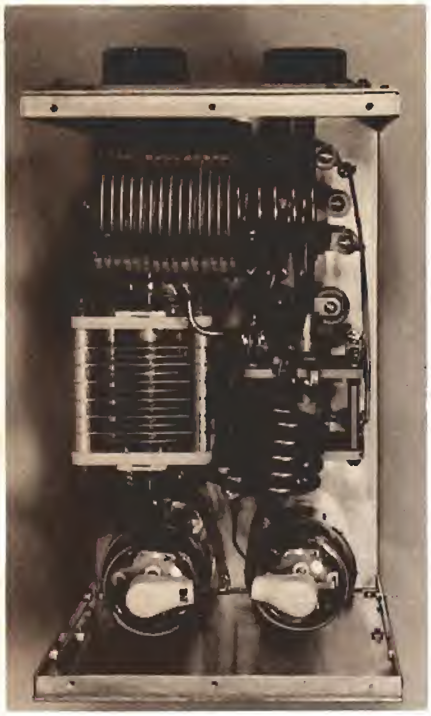
The cathode circuits are metered in the filament center tap. Remember to subtract control grid and screen grid currents from this reading to determine true plate current. Normal cathode current may be read, but it may be abnormal grid current due to drive and loading that is responsible for this reading.

W8DLD also has built an r.f. wattmeter right into this amplifier. The circuit is described in the May-June, 1961 issue. (See LOW-COST RF WATTMETER, page 1.) Forward power up to 500 watts full scale is read in position 1 of $S_3$; and, reflected power up to 50 watts full scale is read in position 2. Thus, readings of nearly 500 watts forward and less than 50 watts reflected power indicate less than 10 per cent reflected power, and a VSWR of less than 2 to 1. The reflected power position can be precisely calibrated with a 50-ohm dummy load.

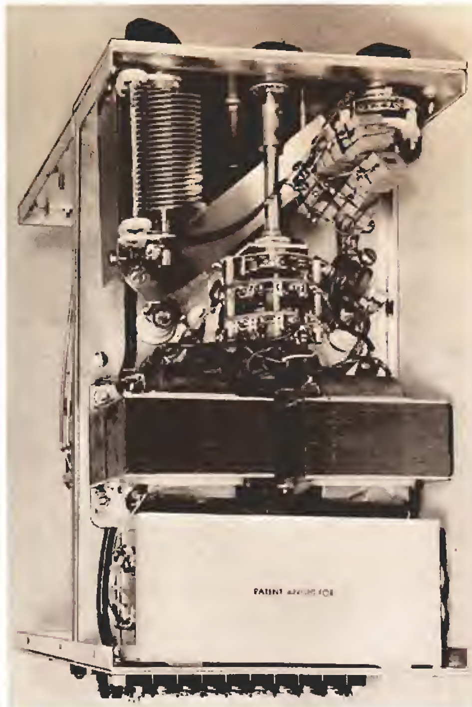
**CONSTRUCTION OF THIS MODEL** was accomplished in a 6 x 10 x 3½-inch deep chassis box (*Bud* CU-3010A Minibox, or equivalent). The parts layout shown in the accompanying pictures and chassis layout drawing, Fig. 2, provides very short r.f. circuit leads and good isolation of the input circuit. Nearly all of the 600 cubic inches of volume in the enclosure are occupied, as readers will note.

The complete enclosure should be constructed first. The 6 x 10-inch end

(continued on page 4)



**TOP VIEW** of the SSB-600 amplifier. Details of tank coil mounting and connections are shown in this view. Allow enough slack in GL-814 plate lead to remove plate caps.



**BOTTOM VIEW,** showing heavy copper strip connections between $C_2$, $S_2$ and the seven 300-mmf. loading capacitors. The FC-30 filament r.f. choke mounts beneath the GL-814 sockets.

**SSB-600** (continued from page 3)

plates were cut from $\frac{1}{16}$-inch thick sheet aluminum. Pieces of ½ x ½ x $\frac{1}{16}$-inch aluminum angle were then fitted to form a flange to which the shield is fastened. About 38 inches of angle stock is required. If sheet metal bending equipment is available, these flanges could be formed on the end plates.

Perforated sheet aluminum (Reynolds or equivalent) about 10⅛ x 20 inches is then folded to form the shield cover, as shown in the pictures. The complete enclosure becomes quite rigid when the shield and bottom cover are in place, despite its light weight. The enclosure is then disassembled, including removing front and back panels, to layout and drill holes for the components. Panel layout is shown in Fig. 3.

After punching and drilling holes for the major components, a shield for the meter ($M_1$) is fabricated as shown in the drawing, Fig. 4, and fastened over the cutout in the chassis to protect the meter from the r.f. field around the plate circuit.

The larger components should be mounted and wired into place. Note that pieces of thin sheet copper flashing have been placed under the chassis between the loading capacitor ($C_2$) and capacitor switch ($S_2$) to provide a low-resistance path for the high r.f. currents in this circuit. Copper strip ½ inch wide is used for connecting leads in this circuit. This pays off in higher efficiency at 21 and 28 megacycles. A copper-clad or solid copper chassis also would help the efficiency, if available.

Components for the r.f. wattmeter should be mounted underneath in the center of the chassis before the meter switch, $S_3$, is assembled. Bypass capacitors and other wiring around the tube sockets are installed before the filament r.f. choke is mounted. Return as many bypass capacitors as possible to a common chassis ground. A terminal strip ($TS_1$) was installed on this model for external power connections, but a suitable multiple-pin jack and plug can be used if desired.

Provision for remote measurement of control and screen grid currents is made by connecting the appropriate current meter between terminals 4 to 7, as follows:

| | | |
|---|---|---|
| 4 to ground: | G-2 (right) | 50 ma. |
| 5 to ground: | G-2 (left) | 50 ma. |
| 6 to ground: | G-1 (right) | 100 ma. |
| 7 to ground: | G-1 (left) | 100 ma. |

**ALL COMPONENTS** in this amplifier have been chosen to handle higher power. Thus, a pair of GL-813 beam pentodes could be substituted for the GL-814's if the chassis is made larger; 7 x 12 x 4 inches (A *Bud* CU-3011A Minibox, or equivalent). However, this size chassis also will hold four type GL-814's in parallel, if anyone prefers to run four of these tubes. Larger filament transformers will be required, of course.

If a pair of GL-813's are used, a well regulated negative bias supply will be required to furnish the approximately minus 70 volts of control grid bias required to hold the plate current to a low value with the triode connection. For this your signal would be 3 DB louder at your friend's receiver. This is less than one S unit. It is frequently easier to gain 3 DB with a little antenna work than by many hours and dollars spent on the linear amplifier.

Some amateurs may want to construct this amplifier as a subassembly to go into a chassis that includes a power supply. This chassis may also include a driver amplifier for use with an exciter delivering less than 50 watts output. When built as an assembly to go into a chassis cabinet arrangement the "do it yourself" enclosure construction is not necessary.

The small package, complete amplifier described herein was constructed because it was meant to serve mainly for mobile operation.

**ADJUSTMENT AND TUNEUP** of this amplifier, after construction is completed, should be done carefully to avoid overloading the tubes for extended periods and thus damaging them. Connect 117 volts AC to terminals 1 and 3, and $J_1$ to an exciter capable of delivering about 50 watts; the output jack, $J_2$, to a 50-ohm dummy antenna load capable of dissipating 500 watts; and the "HV" terminal to a power supply delivering about 1,500 volts DC at 300 ma.

Turn on heater power, high voltage, and apply about 5 watts of driving power at 3.9 megacycles. Set $S_1$ to the 3.5-megacycle position and adjust the plate circuit tuning ($C_1$) and loading ($C_2$) capacitors for maximum output with $S_3$ in position 2 (RF output, forward).

Increase the driving power to about 25 watts and readjust the tuning for maximum output. Then increase the driving power so that 40 milliamperes of grid current is read for each GL-814 in positions 7 and 8 of $S_3$. Again adjust the tuning and loading controls for maximum output. If the amplifier is delivering about 300 watts output, then reduce the driving power a bit and readjust the tuning and loading controls. Output power should be close to the maximum value obtained above.

For test purposes, increase the plate voltage to about 2,400 volts DC and tune carefully for maximum output, running the amplifier for only a minute at a time. It should be possible to obtain 500 watts CW output on all bands from 3.5 to 28 megacycles at 2,400 plate volts, and with a maximum of 40 milliamperes of control grid current per tube. Cathode current will read about 200 milliamperes per tube. At 2,000 to 2,250 plate volts, the amplifier will deliver about 400 watts at 28 megacycles, and 450 watts below 21.5 megacycles.

Frequently it happens that an exciter capable of delivering 100 watts power output into a dummy load will not supply the necessary drive to the cathode circuit of a grounded-

grid amplifier due to an impedance mismatch. A matching network or coupler should then be used between the exciter and amplifier to achieve a match.[3]

**PERFORMANCE** of the amplifier when constructed as illustrated will assure 60% efficiency at 28 megacycles, rising to 70% at 4 megacycles. This may sound high, but the driving power has not been subtracted from the efficiency figure. The amplifier shows a power gain in excess of 10 times. This means that 50 watts should be fed into the input jack if 500 watts output is desired. There is no way to cheat on these figures!

So far this testing has been done under CW conditions. Now the real test comes with an oscilloscope. Connect the scope to the amplifier test output jack, $J_4$. Note the two input and output jacks for easy access to a monitoring spot. Turn on the 500-watt output CW test and set the scope for a good sized CW display. The pattern should be a pure RF carrier. With a grease pencil or crayon, mark the height of this display on the scope screen.

Now switch to SSB and slowly advance the audio gain while speaking into the mike until peaks of the height marked for CW are reached. This indicates that the amplifier is delivering 500 watts peak output. Now adjust the scope for a slow sweep and look at the so called "Christmas tree pattern." Is there any flattening or distortion noticeable at this 500-watt level; or, can the audio level be increased?

If flattening is indicated, plug the scope into the input jack of the linear which will allow monitoring of the exciter. If the same flattening is present, it is coming from the driver. If a display with no flattening is seen, it must be in the linear stage. Try a slight increase in loading by decreasing the load capacitance ($C_2$). Did this cure the flattening? With 50 watts of linear drive, at least 500 watts output without distortion should be seen on the scope. It may be possible to further increase the drive without distortion. Remember that the scope is reading an instantaneous voltage. Also remember that the wattmeter will only read average power and so is of no value for this test.

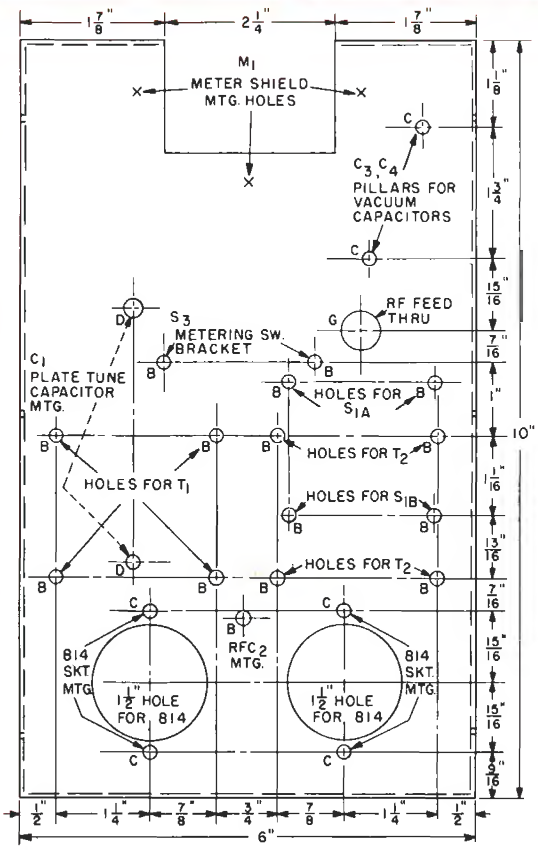
The 500-watt peak output can be directly compared with any other

(continued on page 7)

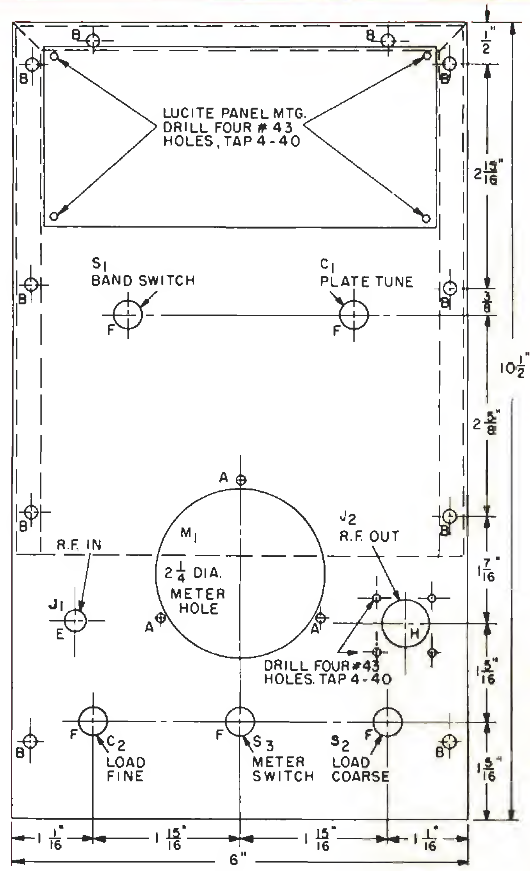
[3]A suitable pi-network impedance matching coupler is described on page 4 of the November-December, 1959 (Vol. 14, No. 6) issue of G-E Ham News.

**TABLE II — DRILL SIZE LEGEND**

"A" drill—No. 31 clears 4-40 screw.
"B" drill—No. 26 clears 6-32 screw.
"C" drill—No. 17 clears 8-32 screw.
"D" drill—No. 9 clears 10-32 screw.
"E" drill—9/32-inch diameter.
"F" drill—3/8-inch diameter.
"G" drill—1/2-inch diameter.
"H" socket punch—5/8-inch diameter for 7-pin miniature tube socket.
"J" socket punch—3/4-inch diameter for 9-pin miniature tube socket.
"K" socket punch—1 1/8-inch diameter for small octal tube socket.
"L" socket punch—1 1/4-inch diameter for large receiving tube socket.




CHASSIS - TOP VIEW




CABINET - FRONT VIEW

**FIG. 2. CHASSIS LAYOUT DIAGRAM,** showing the actual drilling for major parts on W8DLD's model amplifier with two GL-814 pentodes. See TABLE II for the sizes of holes keyed with letters. Locations of small holes marked $C_1$, $C_3$, $C_4$, $RFC_2$, $S_1$, $T_1$ and $T_2$ are for the components actually used, and should be moved to suit components having different mounting dimensions. The cutout for $M_1$ should clear the connecting terminals on the back of the meter.

**FIG. 3. FRONT PANEL LAYOUT DIAGRAM** for the amplifier. The front of the chassis also should be identically drilled, using the panel as a template. Locations for the shafts on $C_1$, $C_2$, $S_1$, $S_2$ and $S_3$ probably will be the same even if similar components are substituted for those specified in TABLE I. Meter mounting holes, marked "A," may differ and should be located from the meter actually used.

# SIMPLIFIED SENSITIVE MULTIMETER

By Charles A. Starks, W2URP

**A SENSITIVE DC MULTIMETER** is always a handy instrument in the amateur radio station. However, complex instruments of this type can be expensive.

"But, they don't have to be," says Chuck, W2URP. "Look at my simple, sensitive DC voltmeter that the average amateur can duplicate in a single evening.

"I needed a DC voltmeter with very high resistance to check and precisely adjust the negative bias on the control grids of the output stage in the new SSB transmitter I added to my station recently. A conventional 1,000 ohms-per-volt meter would have loaded down the circuit excessively and given me a lower-than-actual reading.

"A quick scan through my junk box under the workbench turned up a 100-microampere DC current meter, a sloping panel meter box, and some miscellaneous banana plugs and jacks, terminal boards and hardware.

"A few minutes of figuring with a pencil — after referring to the 'Measurements' chapter of the *Radio Amateur's Handbook* — and I had the multiplier resistance values required for several popular DC voltage ranges. I used the following formula to calculate the multiplier values: $R = \frac{1000E}{I}$; where R is the resistance in ohms; E is the desired full-scale voltage; and I is the full-scale reading of the meter in milliamperes. The 100-microampere meter thus gave a sensitivity of 10,000 ohms per volt.

"Rather than switch in the various multipliers with a tap switch, I decided that each multiplier could be mounted on a terminal board that would plug into the back of the meter case. This provided for future needs by allowing additional ranges to be added at any time."

This is the philosophy with which the Simplified Sensitive Multimeter was designed.

**THE CIRCUIT** of the multimeter is extremely simple, as shown in the schematic, Fig. 1. Multipliers plug into $J_4$ and $J_5$, and the leads running to the circuit to be measured plug into $J_1$ and $J_2$. Provision can also be made to measure currents with this instrument by plugging in a shunting resistance of suitable value across the meter at $J_3$ and $J_5$.

**W2URP** adjusts the control grid bias in his SSB transmitter with his Simplified Sensitive Multimeter. Well-equipped station — and workshop too — includes kilowatt linear amplifier next to SSB transmitter, and matching receiver to right of amplifier. W2URP is an engineer in the Power Rectifier Engineering section of General Electric's Power Tube Department at Schenectady, N.Y. Chuck's favorite bands are 3.9 and 7-MC. SSB, and 7-MC. CW.


**CLOSEUP VIEW** of Simplified Sensitive Multimeter with boards containing multiplier resistors beside it. Shunt for measuring current also can be connected between feedthru terminals, as shown here. CAUTION: Exposed terminals and multiplier strip should be covered with insulation when high voltage circuits are being measured.

**REAR VIEW** of meter showing multiplier board plugged into $J_4$ and $J_5$ on rear of meter box. A multiplier with a single resistor can be made from a narrow strip of insulating board, with the resistor connected between soldering lugs on the plugs.

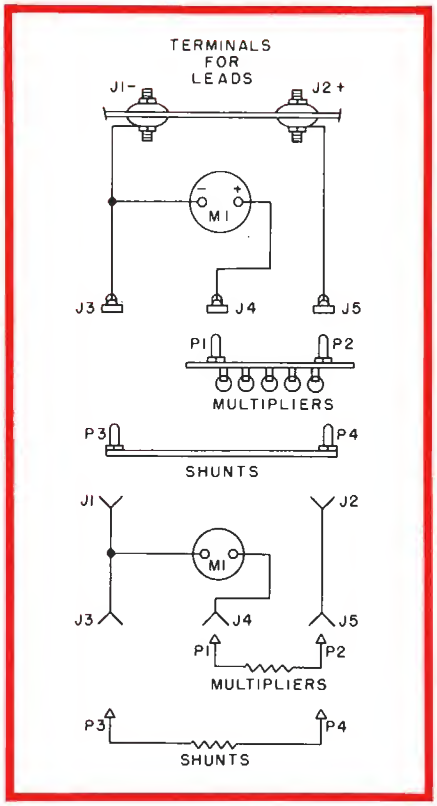



**Fig. 1.** Schematic diagram of the simple multimeter. Terminals $J_1$ and $J_2$ are feedthru insulators with either stud terminals or banana jacks. Jacks $J_3$, $J_4$ and $J_5$ are banana jacks for the multipliers and shunts. Plugs $P_1$ and $P_2$ are mounted on the insulating boards holding the multiplier resistors. Plugs $P_3$ and $P_4$ are on the shunting resistances.

**TABLE I — METER MULTIPLIER CHART**

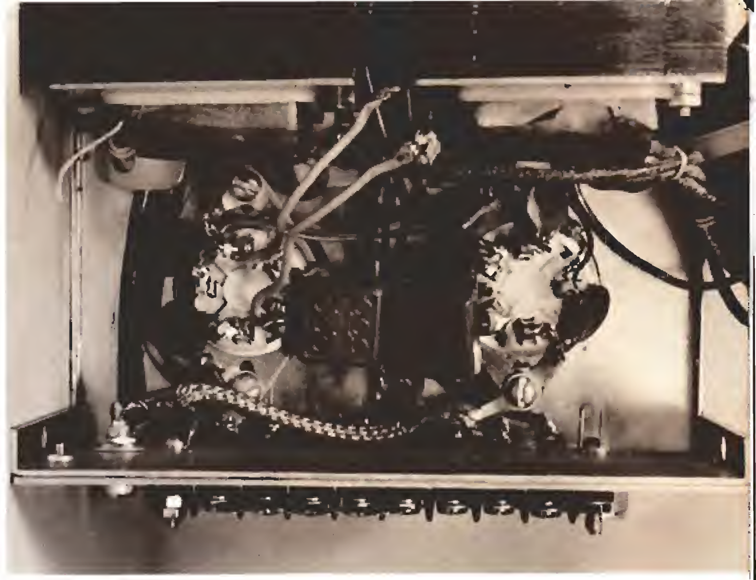
| Full Scale Meter Reading Desired | Multiplier for 20 ua meter | Multiplier for 50 ua meter | Multiplier for 100 ua meter | Multiplier for 250 ua meter | Multiplier for 500 ua meter |
|---|---|---|---|---|---|
| 0.1 Volt | 5,000 ohms | 2,000 ohms | 1,000 ohms | 400 ohms | 200 ohms |
| 1.0 Volt | 50,000 ohms | 20,000 ohms | 10,000 ohms | 4,000 ohms | 2,000 ohms |
| 10.0 Volts | 0.5 megohm | 0.2 megohm | 0.1 megohm | 40,000 ohms | 20,000 ohms |
| 100 Volts | 5 megohms | 2.0 megohms | 1.0 megohm | 0.4 megohm | 0.2 megohm |
| 1,000 Volts | 50 megohms | 20.0 megohms | 10.0 megohms | 4.0 megohms | 2.0 megohms |

### GROUNDED GRID — LINEAR AMPLIFIER — 500 WATTS OUTPUT CW

Parallel connected GL814 tubes — Design data: Min. EP 2000 Max. EP 2500, Optimum EP 2250. For SSB Linear operation load to 300 MA total IP, with 75MA total Igl.

| Meter Switch Position | Reading | Position | Loading Capacity | Band |
|---|---|---|---|---|
| 1 = watts reflected | X50 | 1 = fine | 10 to 325 | 10 |
| 2 = watts forward | X500 | 2 = adds 300 | 325 to 625 | 15 to 20 |
| 3 = Ik MA right 814 | X250 | 3 = adds 300 | 625 to 925 | 20 |
| 4 = Ik MA left 814 | X250 | 4 = adds 300 | 925 to 1225 | 40 |
| 5 = Ig2 MA right 814 | X50 | 5 = adds 300 | 1225 to 1525 | |
| 6 = Ig2 MA left 814 | X50 | 6 = adds 300 | 1525 to 1825 | 75 |
| 7 = Igl MA right 814 | X100 | 7 = adds 300 | 1825 to 2125 | 80 |
| 8 = Igl MA left 814 | X100 | 8 = adds 300 | 2125 to 2425 | |

**INFORMATION** on operating conditions for the GL814 tubes in the SSB-600 grounded-grid linear amplifier. Loading capacitor data and readings obtained in various metering circuits also are given.



**CLOSEUP VIEW** of GL-814 tube sockets with filament r.f. choke removed. Shortest leads are used on bypass capacitors on tube sockets. Capacitors in middle are 0.01-mfd. for r.f. input coupling to tube filaments.

**SSB-600** (continued from page 5)

peak seen on the scope by comparing the amplitude of the deflections in inches or some arbitrary units. Most scopes have translucent graphs permanently attached to the scope face. If yours does not, then attach a temporary one.

If 10 divisions on the scope face equals the 500-watt output calibration, turn up the gain until 12.2+ divisions of clean output is read. How many peak watts output is it? Remember $\frac{E^2}{R}$=watts output and the "R" in this case is a constant so the $E^2$ can be related directly to watts. If the first E reading equals 10, the first $E^2$ equals 100. Therefore, 100—500 watts. If the second E reading equals 12.2+, the second $E^2$ equals 150 in round numbers. Now by the simple proportion 100:150 equals 500:X, the 12.2+ scope reading represents 750 watts peak. If your scope shows a reading on this arbitrary scale of 14+, it will be indicating a nice 1-kilowatt peak power output. Remember that when using a scope, voltage is being measured. In a given circuit, when the voltage indication doubles, the power has quadrupled. When the power in an antenna is multiplied by four, it equals 6 decibels increase in signal strength, or one big "S" unit.

All things considered, the SSB-600 linear amplifier will do a man-size job if you build it right, tune it right, and most important, operate it right!

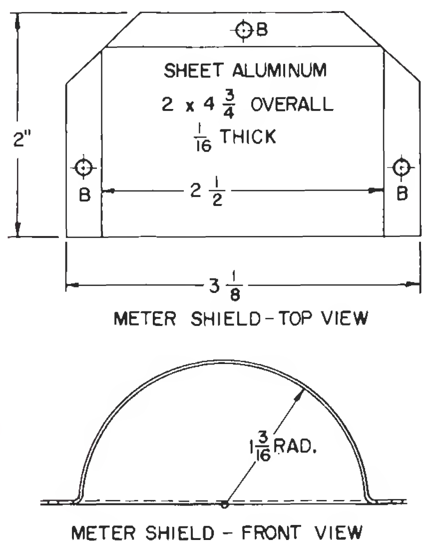



**FIG. 4. DETAIL VIEW** of the metal shield which goes over the top of the meter to protect it from the plate circuit r.f. field.

Meters having several different full-scale current ranges were tried in this circuit at W2URP. Values of the multiplier resistances required to obtain several popular full-scale voltage readings with meters rated at from 20 to 500 microamperes have been tabulated in TABLE I — METER MULTIPLIER CHART. Multipliers may be assembled from two or more resistances in series to obtain the required total resistance. Five such resistances were used for the multipliers in the model constructed by W2URP.

Precision 1-percent tolerance resistances assure the best accuracy, but inexpensive composition resistors may be combined in series to obtain the correct total resistance. By selecting values carefully, the tolerances in the inexpensive resistors can thus be made to cancel each other out, resulting in a precise total value of resistance.

Shunting resistances will range from a fraction of an ohm, to a few ohms, depending upon the full-scale current range desired. They can be made from either nichrome resistance wire, or copper wire.

The exact value of shunting resistance can be determined by plugging an insulated board into $J_3$ and $J_5$, and then connecting a short length of wire between $P_3$ and $P_1$. A current of the desired full-scale value is then passed through the meter, and the wire is shortened or lengthened until the meter shows a full-scale reading. Shunts having a few inches of wire may be wound on 47-ohm, 1-watt composition resistors.

**CONSTRUCTION DETAILS** are shown in the illustrations on this page. The meter cases usually have feedthru insulators already in place. Obtain a case with a hole to fit the size of meter that will be used.

All banana jacks on the rear of the case should be insulated with the fiber washers provided with the jacks. These washers are usually adequate for several hundred volts. Wiring inside the case is run with insulated hookup wire. Standard test prods are connected to $J_1$ and $J_2$ on top of the case.

Multipliers are mounted on insulated terminal boards, and fitted with banana plugs spaced to match the multiplier jacks on the meter case. A separate multiplier board is required for each voltage range.

The meter is used in the same manner as a regular multimeter. Polarity of the meter must be observed. Before checking an unknown voltage, be sure to plug in a multiplier for a full scale reading higher than the voltage is likely to be. When storing the meter, plug in a low-resistance shunt across the meter.

This simple multimeter will provide measurements of voltage accurate to within a few percent in circuits where the circuit resistance is up to 15 percent of the full-scale resistance of the multimeter. When constructed with a meter having a full-scale sensitivity of 100 microamperes or less, it will provide useful measurements of voltage in receiver and other low-level circuits.

SCANNING THE SPECTRUM

# 1960 EDISON RADIO AMATEUR AWARD

## THE EDISON RADIO AMATEUR AWARD

. . . was established in 1952 by the General Electric Company to provide for public recognition of the many outstanding public services performed by radio amateurs. Many such commemorable events go unnoticed each year which otherwise could raise the stature and prestige of all radio amateurs.

The Award is presented annually to a licensed radio amateur who, while pursuing his or her hobby within the limits of the United States, has performed an outstanding meritorious service in behalf of an individual, group, or the general public.

These services range from providing vital emergency communications during emergencies, often in dangerous situations, to organizing compex communications systems, and unique services to an individual.

Candidates for the Award are nominated by letter from individuals, or clubs, associations and other groups familiar with the public service performed by their candidate.

The recipient is selected at the end of January by a panel of distinguished and impartial judges from among candidates nominated by persons familiar with the service each candidate has rendered.

Ralph E. Thomas, KH6UK

John T. Chambers, W6NLZ

. . . whose trans-Pacific experiments have set distance records and opened new horizons in UHF communications, have been chosen jointly by the Judges to share the 1960 Edison Radio Amateur Award for outstanding service.

This year marks the first time the award has been granted for scientific achievement. Messrs. Thomas and Chambers have devoted four long years to patient and often fruitless experimentation with tropospheric ducting radio propagation phenomena, culminating in a one-way communications distance record of 2,540 miles on the 432 megacycle amateur band.

This and earlier two-way records set over the same California-to-Hawaii path on 220 and 144 megacycles confirmed the theory that UHF radio communications were not limited to line of sight. Their work has stimulated commercial and military interest and experimentation in communication via this phenomena.

The judging panel, in comparing their acomplishments to the first trans-Atlantic radio communications in the 1920's, noted that the work of Messrs. Thomas and Chambers further enhances the standing of amateur radio operators in the scientific world.

Judging centers on the greatest benefit to an individual, group, or community, and the amount of ingenuity, devotedness and sacrifice the candidates display in performing their services.

The presentation of the Edison Radio Amateur Award trophy and a check for $500 to the recipient is made several weeks later at a ceremony in Washington, D. C., before prominent figures in military, government and civilian communications.

*Judging the 1960 Edison Award —*

E. ROLAND HARRIMAN
*Chairman*, American National Red Cross.

ROSEL H. HYDE
*Commissioner*, Federal Communications Commission.

GOODWIN L. DOSLAND
*President*, American Radio Relay League.

GE TUBES HAM NEWS

MARCH-APRIL 1961
VOL. 16, No. 2